

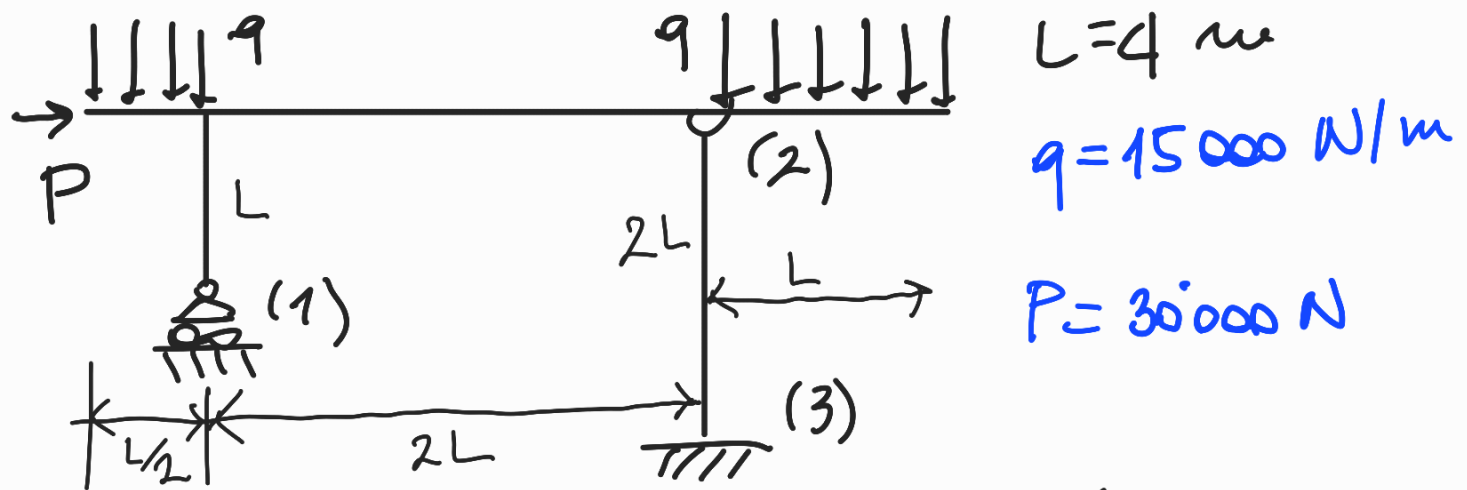
1) • Verifica che la struttura è isostatica

$$n_{\text{aste}} = 2$$

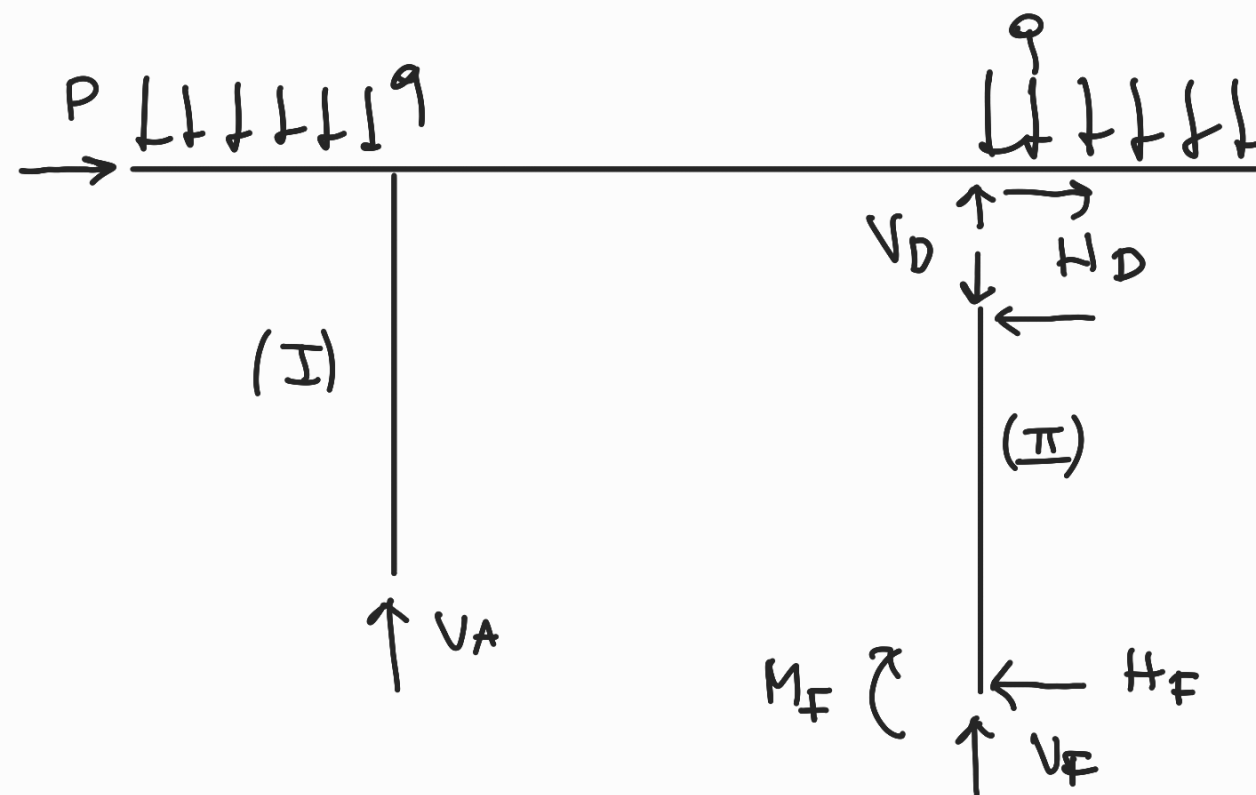
$$v = 3 + 2 + 1 = 6$$

$$g = 2 \cdot 3 = 6$$

→ isostatica



• Calcolo delle reazioni vincolari



Equilibri delle aste:

$$I \begin{cases} \rightarrow + P + H_D = 0 \\ \uparrow V_A - q \frac{3}{2} L + V_D = 0 \\ \curvearrowright_D : V_A \cdot 2L - q \frac{L}{2} \cdot \frac{9L}{4} + q \frac{L^2}{2} = 0 \end{cases}$$

$$H_D = -P = -30000 \text{ N}$$

$$V_D = \frac{3}{2} qL - V_A = 71250 \text{ N}$$

$$V_A = 18750 \text{ N}$$

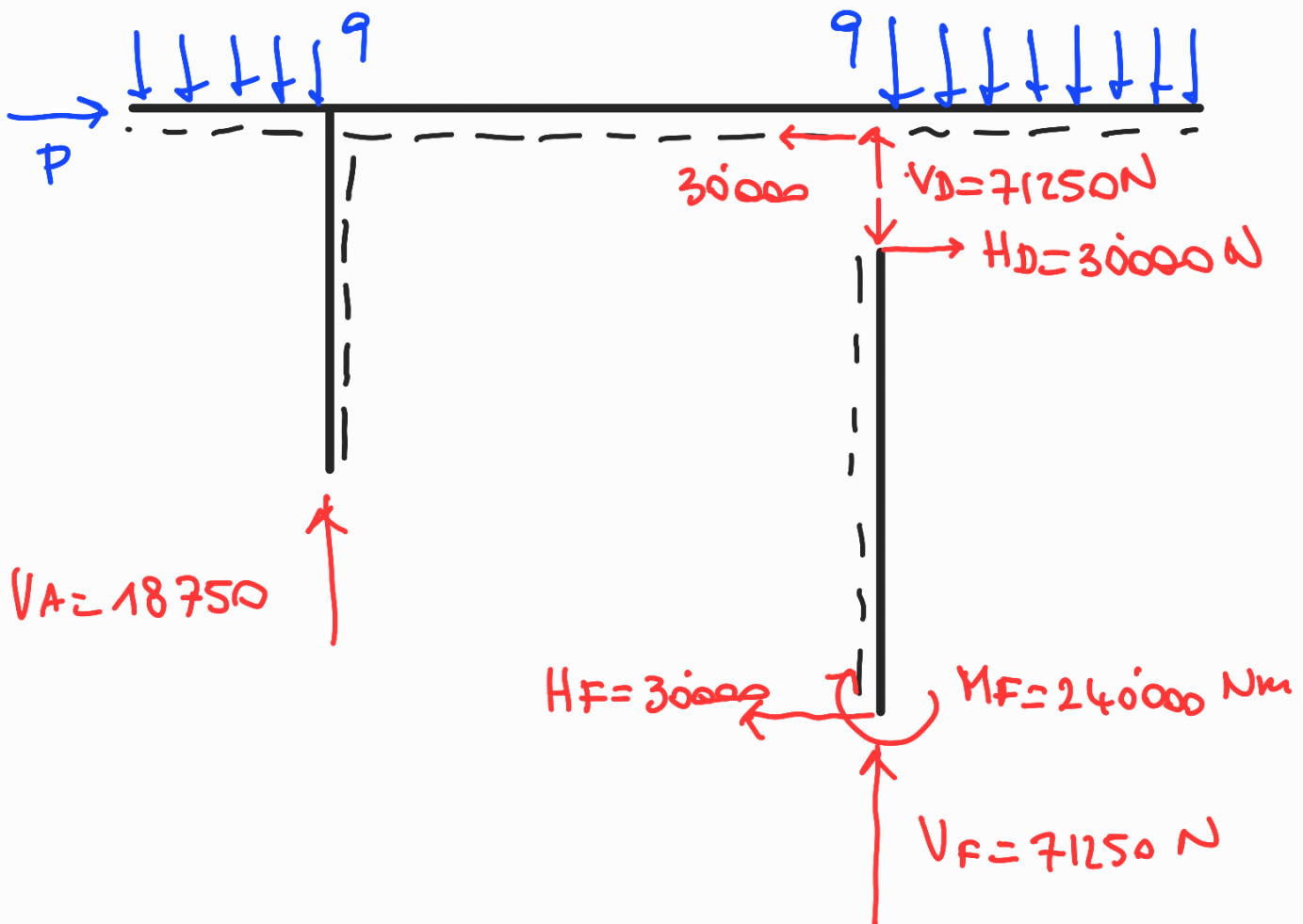
$$II \begin{cases} \rightarrow + -H_D - H_F = 0 \\ \uparrow V_F - V_D = 0 \\ \curvearrowright_F : M_F - H_D \cdot 2L = 0 \end{cases}$$

$$H_F = -H_D = 30000 \text{ N}$$

$$V_F = V_D = 71250 \text{ N}$$

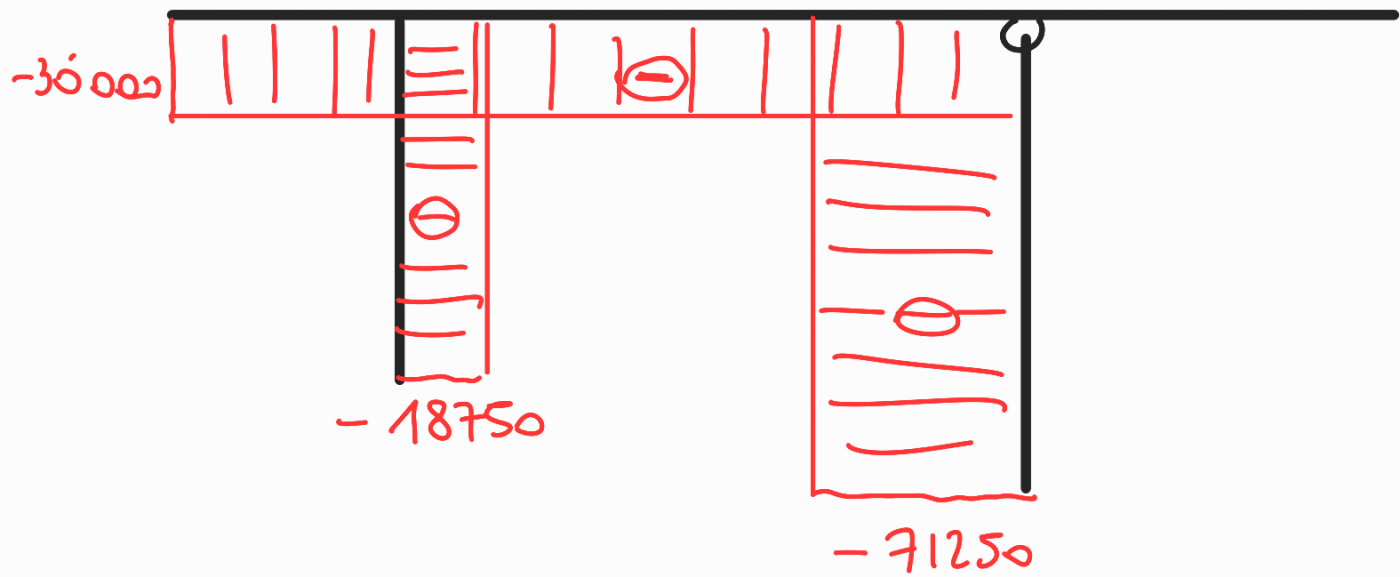
$$M_F = H_D \cdot 2L = 240000 \text{ Nm}$$

Schema finale delle forze attive e reattive

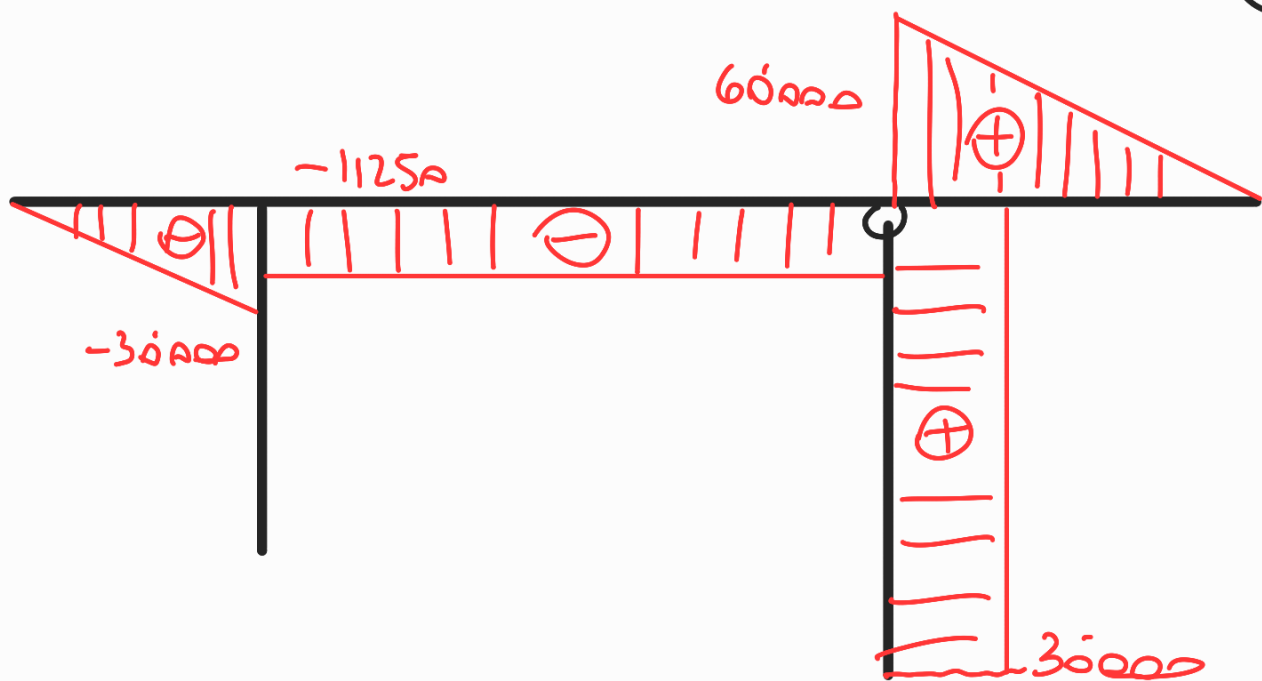


• Diagrammi delle azioni interne

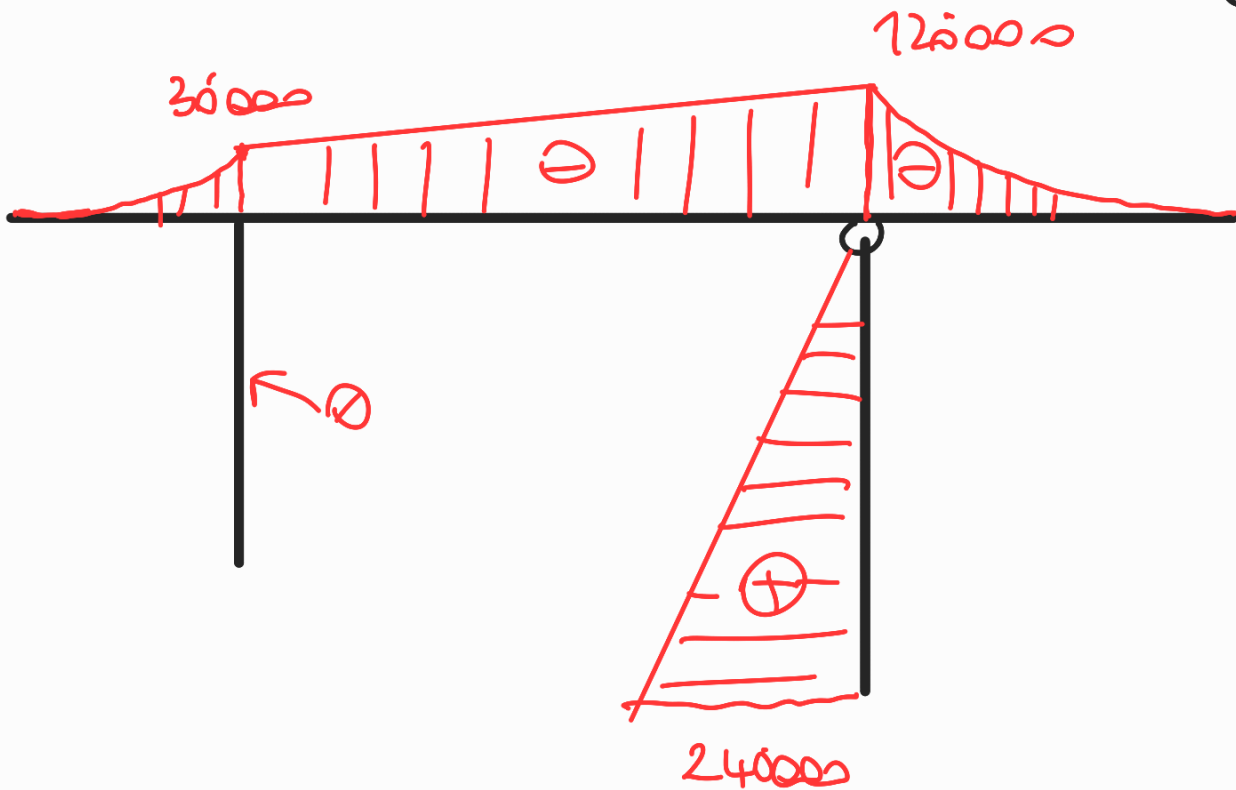
(2)



(T)

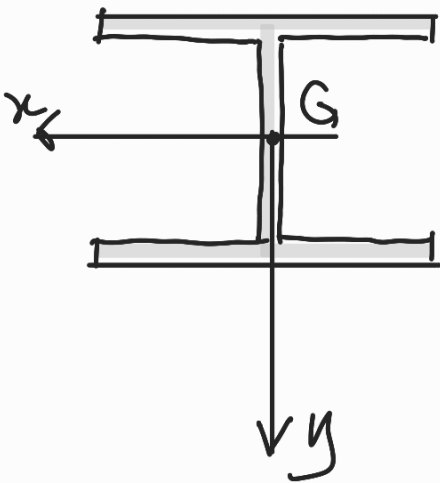


(M)



2)

• Caratteristiche geometriche della sezione



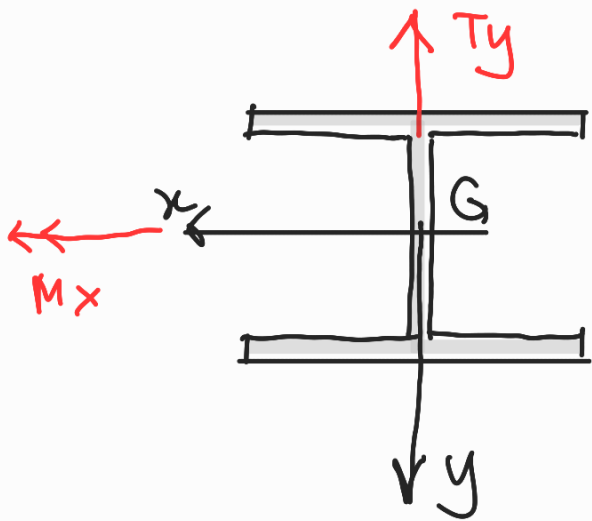
$$A = 6(0,2 \cdot 0,015) = 0,018 \text{ m}^2$$

$$I_x = \frac{0,015 \cdot 0,4^3}{12} + 2 \cdot 0,4 \cdot 0,015 \cdot 0,2^2 = 5,6 \cdot 10^{-4} \text{ m}^4$$

Il momento di inerzia I_y non è

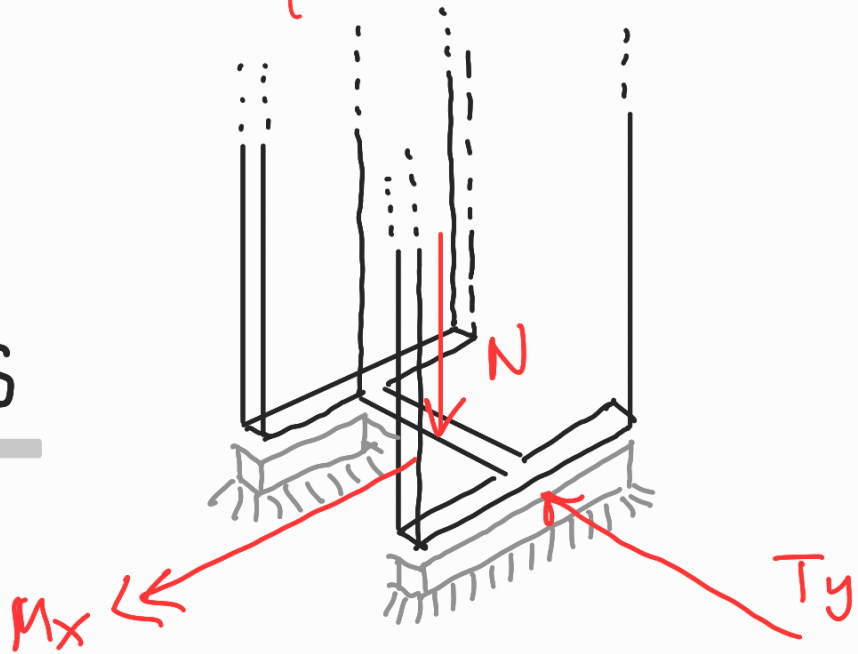
necessario.

● Calcolo delle Tensioni nelle sez. S

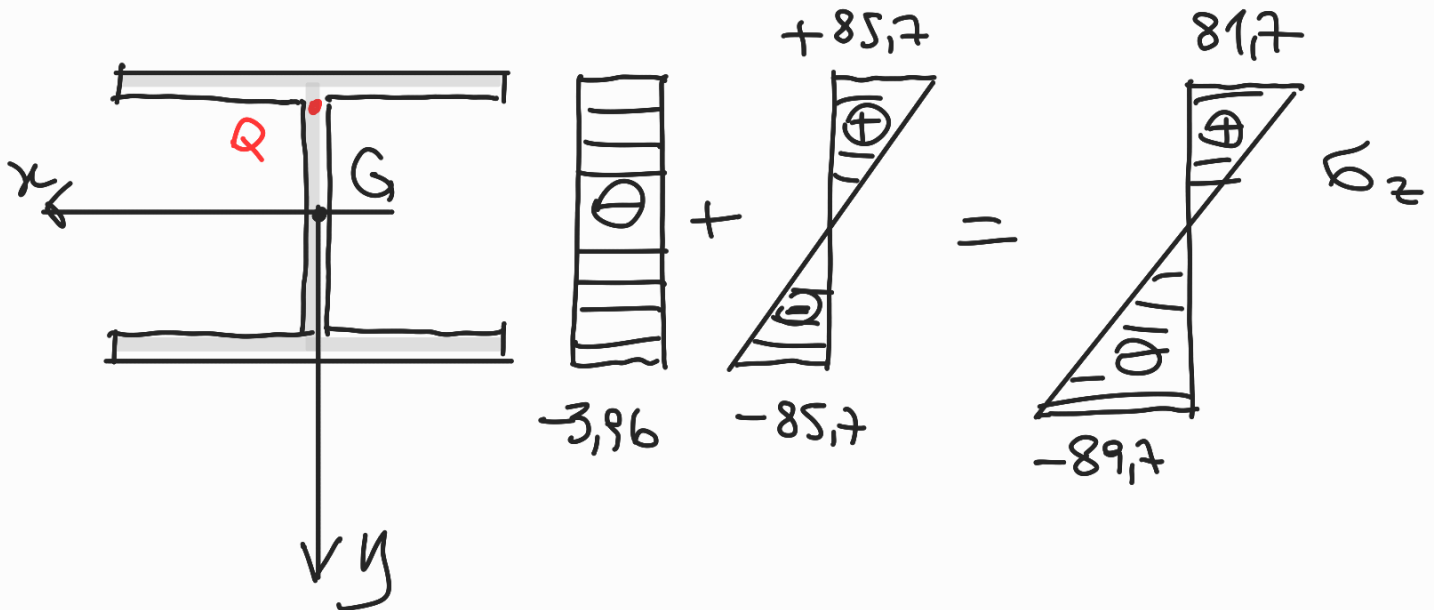


$$\left. \begin{aligned} N &= -71250 \text{ N} \\ T &= 30000 \text{ N} \\ M_x &= 240000 \text{ Nm} \end{aligned} \right\}$$

Sez. S-S



● Sforzo normale eccentrico



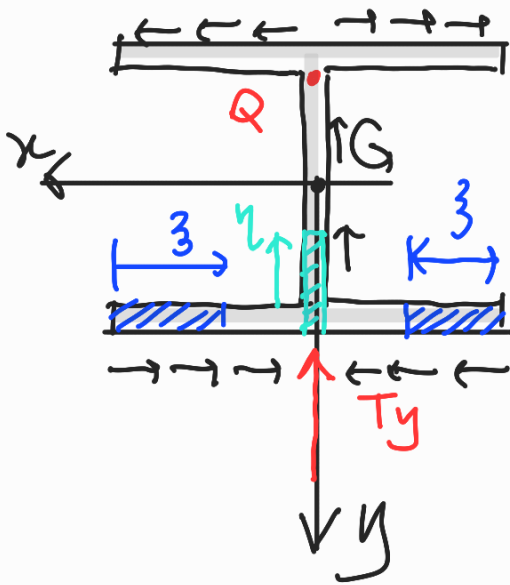
$$\sigma_z(y) = \frac{N}{A} \pm \frac{M_x}{I_x} \cdot y$$

$$= \frac{-71250}{0,018} \pm \frac{240000}{5,6 \cdot 10^{-4}} \cdot y =$$

$$= -3,96 \cdot 10^6 \pm 85,7 \cdot 10^6 = \begin{cases} -89,7 \text{ MPa} \\ +81,7 \text{ MPa} \end{cases}$$

$$\sigma_z(Q) = -95,5 \text{ MPa}$$

● Taglio (f. di Jourawski) $\tau_{zs} = -\frac{T_y S_x^*}{I_x \cdot b}$



$$\tau_{zx}(z) = -\frac{T_y \cdot 2z \cdot t \cdot a}{I_x \cdot 2t}$$

$$\tau_{zx}(z=0,2) = \frac{30000 (0,2 \cdot 0,015 \cdot 0,2) \cdot 2}{5,6 \cdot 10^{-4} \cdot 2 \cdot 0,015} = 2,14 \cdot 10^6 \text{ Pa}$$

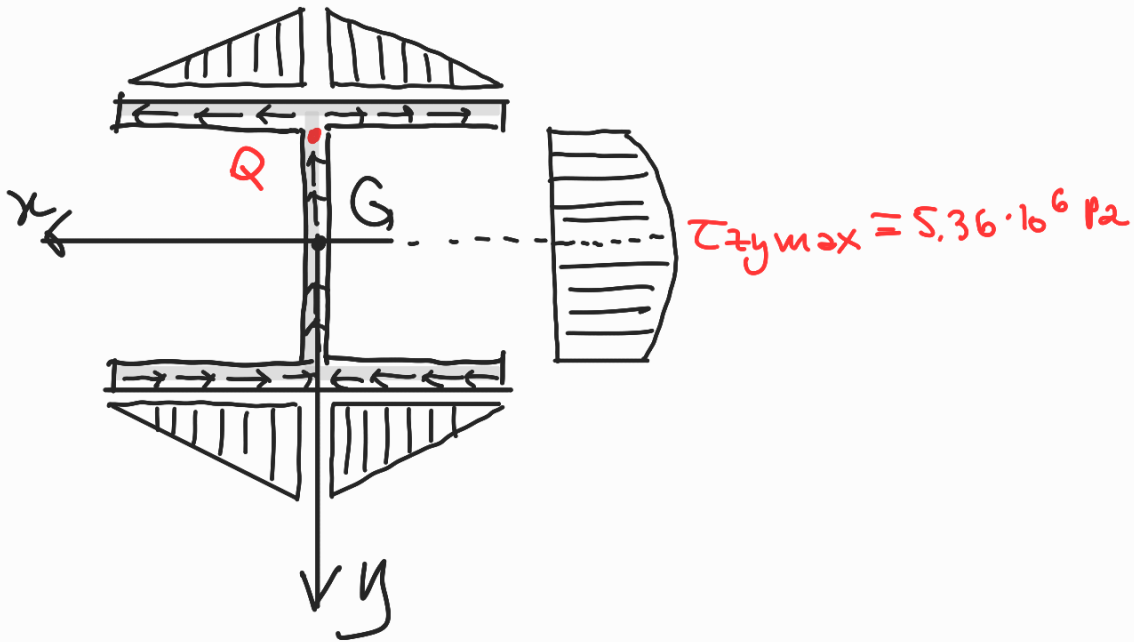
ascendente

$$\tau_{zy}(y) = -\frac{T_y \left[2 \cdot 0,2 \cdot 0,015 \cdot 0,2 + y \cdot 0,015 \cdot \left(a - \frac{y}{2} \right) \right]}{5,6 \cdot 10^{-4} \cdot 0,015}$$

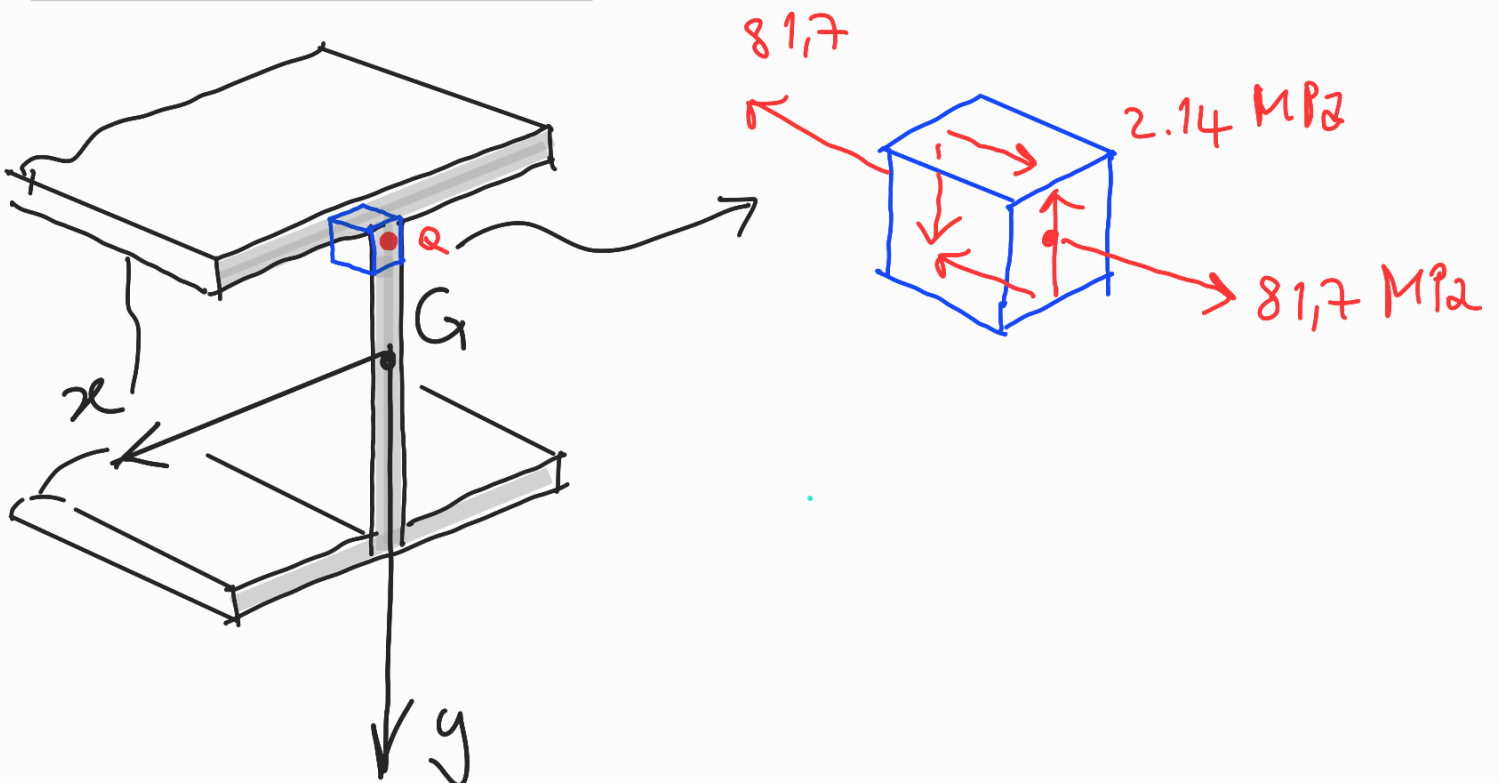
$$\tau_{zy}(y=0,2) = \frac{30000 \cdot 1,5 \cdot 10^{-3}}{5,6 \cdot 10^{-4} \cdot 0,015} = 5,36 \cdot 10^6 \text{ Pa}$$

$\tau_{zy \max}$

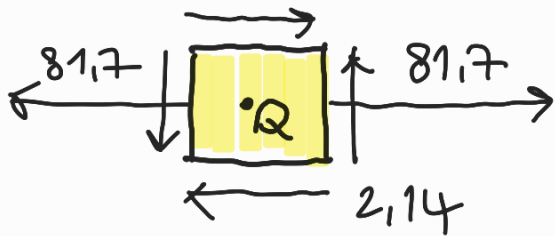
$$\tau_{zx}(Q) = 2,14 \cdot 10^6 \text{ Pa}$$



- Verifica di resistenza nel punto Q delle set S
e cerchio di Mohr

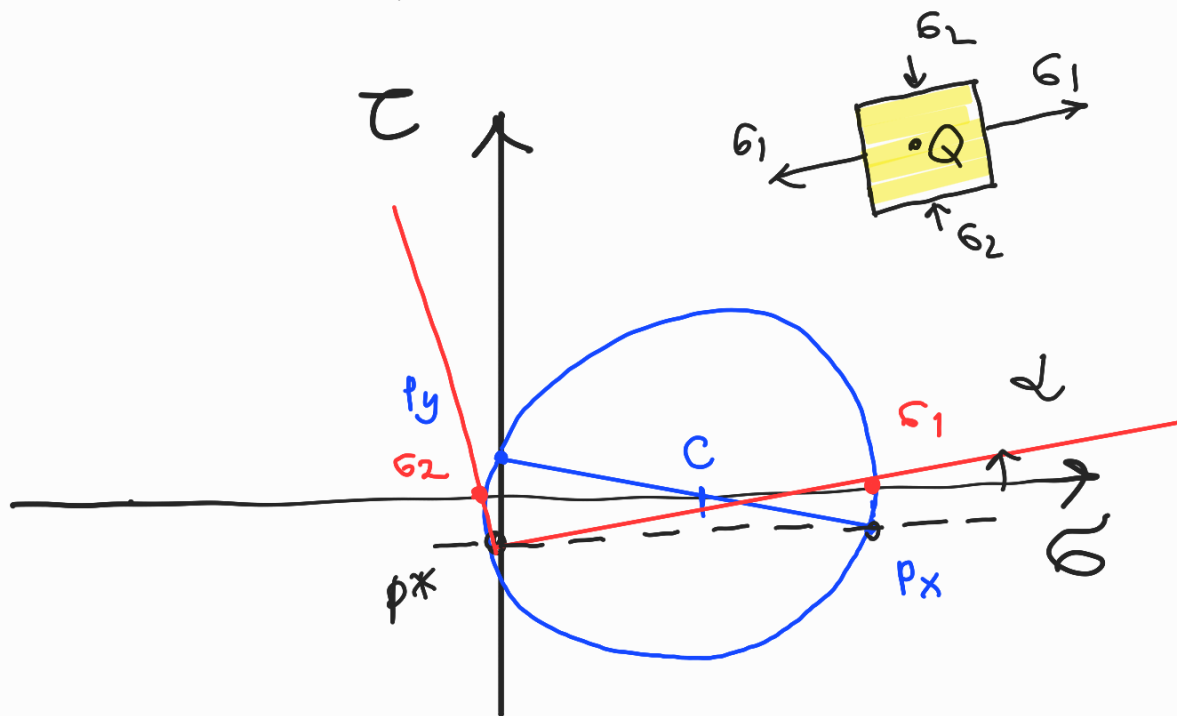


Punto Q (MPa)



$$P_x = (81,7 ; -2,14)$$

$$P_y = (0 ; 2,14)$$



$$x_c = +40,85 \text{ MPa} \quad r = 40,90 \text{ MPa}$$

$$\begin{cases} \sigma_1 = x_c + r = 81,75 \text{ MPa} \\ \sigma_2 = x_c - r = -0,05 \text{ MPa} \end{cases}$$

$$\alpha = \frac{1}{2} \arctg \frac{\tau_{xy}}{\frac{\sigma_x - \sigma_y}{2}} = +1,5^\circ \quad \text{antiorario}$$

• Verifica di resistenza nel punto Q

Criterio di Von Mises

$$\sigma_{eq. VM} = \sqrt{\sigma^2 + 3\tau^2}$$

$$\sigma_{eq. VM} = \sqrt{81,7^2 + 3 \cdot 2,14^2} = 81,78 \text{ MPa} < 160 \text{ MPa}$$

Verificato

